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<b>(54) Title:</b> DETERMINATION OF PARTICLE SIZE AND ELECTRIC CHARGE  <b>(57) Abstract</b> <p>A method for the determination of particle size and electric charge or zeta potential of particles dispersed in a fluid medium. The particle size and charge are determined from measurements of (1) the phase lag between an applied alternating electric field and the resulting particle velocity, and (2) the amplitude of the particle velocity. Also disclosed is the measurement of the interaction of sound waves and electric fields in the fluid medium over a range of frequencies to obtain the particle size and zeta potential.</p>		

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DETERMINATION OF PARTICLE SIZE AND ELECTRIC CHARGETECHNICAL FIELD

The present invention relates to a method of and means for the determination of particle size and electric charge or zeta potential in a colloidal system.

A colloid is a suspension of small particles in a fluid medium (e.g. aerosols and the dispersions of solids in liquids). Colloids have great scientific and industrial importance. Examples include blood, paints, slurries and milk.

The most significant characteristics of many colloidal systems are the size and charge of the particles, since most other properties of the system are influenced to some extent by these factors.

There are many areas of industry in which it is necessary to be able to determine the size of particles suspended in a liquid or the electric charge on the particles. For example, in the mining industry, mineral ores must be ground down until the particles are the right size for floating, and in liquid purification processes it is important to be able to keep particle charge low in order to encourage the coagulation of the particles into clumps large enough to be filtered out.

In nearly every colloidal system the particle carries an electric charge. This charge is balanced by an excess of ions of opposite charge in the suspending liquid. These ions tend to cluster around the particle, forming a

diffuse cloud which is known as the double-layer. The voltage difference between the particle surface and the liquid beyond the double-layer in equilibrium is referred to as the "zeta potential" denoted by  $\zeta$ . The bigger the particle charge, the bigger the  $\zeta$  potential.

#### BACKGROUND ART

Known methods for measuring particle size include the use of electron microscopes, Coulter counters, centrifuges and dynamic light-scattering devices. However, all of these known methods require the removal, and subsequent dilution of the sample prior to testing, making such methods unsuited to on-line monitoring of particle size.

Known methods for measuring particle charge all involve the measurement of the particle velocity in an electric field. In some methods, the velocity is determined by measuring the time required for the particle to pass between two points on a microscopic grid when a steady electric field is applied. In other methods, particle velocity is measured by a light-scattering technique with an alternating electric field of 10 or 20 Hz.

There is apparatus suitable for determining both particle size and charge. The "zeta Sizer" (Malvern Instruments) measures the light scattered from a laser beam as it passes through the suspension. In the absence of an applied field, the fluctuations in the scattered light provide information about the particle size, and if a slowly

varying electric field is applied the particle charge can be obtained from the fluctuating light signal.

All of the above methods suffer the disadvantage that they require sample dilutions and most require use of light-scattering instruments. Accordingly, opaque samples cannot be measured.

#### DISCLOSURE OF THE INVENTION

It is an object of the present invention to provide a method of and means for the determination of particle size and electric charge or zeta potential of particles in a colloidal system.

It is another object of the present invention to provide a method of and means for the determination of particle size and electric charge or zeta potential of particles in a colloidal system on-line and without sample dilution, even in opaque solutions.

It is a further object of the present invention to provide a method of and means for determination of the motion of colloidal particles in a high-frequency field, for it is by the use of high frequency measurements of particle motion that the particle size and charge can be determined.

These and other objects of the present invention will be apparent from the following non-limiting disclosure of the invention.

According to one aspect of the present invention there is provided means for determining the size and charge of particles dispersed in a fluid medium from the phase lag

and amplitude of particle velocity in an alternating electric field.

According to a further aspect of the present invention there is provided means for determining the particle size in a fluid medium having uniform, low potential from a measurement of the phase of the particle motion in a high frequency alternating electric field, and wherein the zeta-potential can be determined from the amplitude of the motion in the alternating field.

According to another aspect of the invention there is provided a means for determining the particle motion in an alternating field from measurements of the interaction of sound waves in the suspension.

According to a further aspect of the invention there is provided means for measuring and generating the interaction of sound waves and electric fields in a suspension, comprising positioned spaced apart electrodes and pressure transducers in contact with the suspension, enabling the simultaneous measurement of electric current, potential, and pressure differences in the suspension.

These and other aspects of the invention will be apparent from the above, and from the following description relating to the invention.

#### BRIEF DESCRIPTION OF THE DRAWINGS

The invention will be further described with reference to the drawings, in which:-

Figure 1 illustrates separate graphs of applied

electric field versus time and particle velocity versus time;

Figure 2 illustrates graphically the determination of particle size from phase lag measurement;

5 Figure 3 illustrates graphically the subsequent determination of particle charge from amplitude measurement; and

Figure 4 illustrates a parallel plate cell used in obtaining measurements in some embodiments of the present  
10 invention.

#### MODE FOR CARRYING OUT THE INVENTION

When an alternating electric field is applied to a colloidal suspension it causes the particles to oscillate at the frequency of the applied field in a way which depends  
15 on particle size and zeta potential. If the frequency of the applied field is much lower than the optimum sizing frequency (to be defined hereinafter), the particle velocity will be in phase with the applied field; i.e., when the field switches direction, so too does the particle motion.  
20 At higher frequencies a phase lag develops, i.e., there is a time lag between the change in direction of the applied field and the subsequent change in the direction of the particle motion due to the particle inertia. This is illustrated in Figure 1.

25 For a given particle, the phase lag increases with particle radius (since this increases the particle inertia), while the velocity amplitude decreases with

radius. In general these two quantities also depend on particle  $\zeta$  potential. Thus by measuring phase lag and amplitude it should be possible to determine size and charge.

5 For suspensions in which the particles have a uniform, low  $\zeta$ -potential it is shown that the phase lag is independent of the magnitude of  $\zeta$ . For such suspensions a measurement of phase lag can therefore be used to determine particle size, and the amplitude measurement can then be  
10 used for charge determination. Mathematical formulae relating phase lag to particle size, and amplitude to size and charge are presented for a dilute suspension of spheres with low  $\zeta$ . The particle velocity can be obtained indirectly from measurements involving the interaction of  
15 electric fields and sound waves in the suspension. It can for example be obtained for the measurement of sound waves generated by electric fields, or from the measurement of electric fields generated by sound waves in the suspension. An advantage of the present invention is that measurement  
20 can be performed on-line, as opposed to the sampling methods required of the prior art and it can be applied to opaque suspensions. The present invention can also be applied to larger particles than can the prior art light scattering techniques, which are limited to  $<1\mu\text{m}$  range. In the case of  
25 highly charged particles, it may be necessary to reduce the charge by the addition of salt or acid/base, since the determination of size and charge is simpler for systems with



low  $\zeta$ -potential. Alternatively, high  $\zeta$  systems can be sized by using a prior calibration procedure.

The only theoretical studies of particle velocity that have appeared in the literature have been concerned with either a steady electric field ("Zeta Potential in Colloid Science" by R.J. Hunter, Academic Press 1981, Chapter 3) or an alternating field at frequencies which for most suspensions are well below the optimum frequency for size determination (Hinch E.J., et al, J. Chem. Soc. Faraday Trans. 2 80, 535 (1984)). The latter authors made no mention of the possibility of size determination from phase lag and amplitude measurement.

In accordance with the present invention particle velocity has been calculated for a dilute suspension over the frequency range which is best-suited to particle sizing, that is frequencies of the order of  $\nu/a^2$ , where  $\nu$  is the kinematic viscosity of the suspending liquid ( $\approx 0.01 \text{ cm}^2/\text{sec}$  for water), and  $a$  is the particle radius. For an  $0.1 \mu\text{m}$  radius particle, this optimum frequency is 16 MHz. In this frequency range the phase lag is a sensitive function of frequency, and for this reason it is well-suited for determining particle sizes.

As indicated above, the particle velocity can be determined by measuring the interaction of sound waves and electric fields in the suspension; it can for example be determined by measuring sound waves generated by an alternating electric field, and by measuring the electric

fields generated by sound waves. Of these two effects, only the second has appeared in the scientific literature. Most of the work on this effect is restricted to electrolytes, with the most notable exception being two papers by J.A. Enderby (Proc. Roy. Soc. A 207, 329 (1951)) and J.A. Enderby and F. Booth (Proc. Phys. Soc. 65, 321 (1952)). These authors apparently had no idea that this effect was related to the particle velocity. Furthermore, there appear to be a number of errors in their work R.W. O'Brien, J. Fluid Mech. (to be published). There is no disclosure in these references of the possibility of obtaining particle size from this effect.

The phenomenon of sound wave generation by an electric field is described in U.S. Patent 4,497,208. However, there is no disclosure in the above referenced patent of the link between the effect and particle velocity, or of the possibility of determining particle size from the effect.

Formulae associated with particle size and charge  
20 determination

There are two main aspects to this invention:

- (1) A method for determining particle size and charge from measurements of particle velocity in an alternating electric field
- 25 (2) A method for obtaining that particle velocity from measurements of the interaction of sound waves and electric fields in the suspension.

With the aid of these procedures it is possible to determine particle size and charge from measurements of the interaction of sound waves and electric fields in any suspension.

5 Aspect (1) of the invention will be described in the following two sections. Aspect (2) will be addressed in section 3.

1. The velocity of an isolated sphere in an alternating electric field.

10 In a dilute suspension, each particle can be treated as being alone in an infinite liquid. In this section a dilute suspension of uniform spheres will be studied. We let  $\underline{E}_0 \cos wt$  denotes the ambient electric field in the suspension; this is the electric field which would  
15 apply in the absence of any particles.  $|\underline{E}_0|$  is the amplitude of this applied field, and  $w/2\pi$  is the frequency.

Following the standard procedure for problems involving sinusoidally varying quantities, this applied field can be rewritten as  $\underline{E}_0 e^{iwt}$ , with the understanding  
20 that the field is actually given by the real part of this complex expression.

Since colloidal particles are electrically charged, the applied field exerts an alternating force on the particles which causes them to oscillate backwards and  
25 forwards at the frequency of the applied field. The particle velocity is denoted by  $\underline{v}_0 e^{iwt}$ . The complex quantity  $\underline{v}_0$  requires two real numbers (and a direction) for

its specification. The two numbers are  $|\underline{V}_0|$ , the amplitude of the particle velocity, and  $\arg \underline{V}_0$  the phase lag referred to earlier.

The quantity  $\underline{V}_0$  is proportional to  $\underline{E}_0$ , the strength of the applied field. For spherical particles, which on account of their symmetry move in the direction of the applied field, this proportionality relation takes the simple form

$$\underline{V}_0 = \mu \underline{E}_0 \quad (1)$$

The phenomenon of particle motion in an electric field is called "electrophoresis", and  $\mu$  is termed the "electrophoretic mobility" of the particle. Like  $\underline{V}_0$ ,  $\mu$  is a complex quantity.  $|\mu|$  is equal to  $|\underline{V}_0|$  for unit applied field, and  $\arg \mu$  is equal to the phase lag. Since  $\mu$  is independent of  $\underline{E}_0$ , it can only depend (for any given frequency) on the properties of the particle and solvent;  $\mu$  is the quantity which should be measured in the course of determining particle size and charge.

The calculation of  $\mu$  is greatly complicated by the fact that the applied field distorts the double layer. As a result the double layer ions impose an electric force which retards the particle, thereby affecting both the phase lag and the amplitude of the motion. Fortunately, at the optimum sizing frequency, this double-layer distortion can be neglected in the important case of particles with low  $\epsilon$

potential.

The range of validity of this low- $\zeta$  approximation depends on the ratio of particle radius to double-layer thickness; If that ratio is around one, the approximation should be valid for  $\zeta$  potentials of up to about 50mv. If particle radius is much greater than double-layer thickness, the  $\zeta$  potential limit will be larger; For example, if the ratio of the radius to thickness is 50, the low- $\zeta$  approximation will work up to about 100mv. This should cover most commonly occurring colloids. For the highly charged colloids it may be necessary to add salt or acid/base to reduce the  $\zeta$  potential and thereby take advantage of the low- $\zeta$  results.

For a sphere with low  $\zeta$ , we have shown that the electrophoretic mobility is given by the formulae

$$|\mu| = \frac{4\pi\epsilon}{3} |\zeta| |G|, \quad (2)$$

3

$$\arg \mu = \pi (u(\zeta) - 1) + \arg G, \quad (3)$$

20

where

$$G = \kappa^2 a e^{\kappa a} \left( \frac{V'}{F'} \right) \left\{ \frac{3e^{-\kappa a}}{\kappa} \left[ a + \frac{1}{\kappa} \right] - \frac{6bc}{a} E_5(\kappa a) + 2a \left| \frac{-ik}{ik-\kappa} e^{(ik-\kappa)a} + ca^3 \left( \frac{ik}{a^2} E_3(-ika + \kappa a) - \frac{3}{a^3} E_4(-ika + \kappa a) + \frac{3}{ika^4} E_5(-ika + \kappa a) \right) \right| \right\}. \quad (4)$$

Here  $E_n$  is the exponential integral

$\epsilon$  is the permittivity of the suspending liquid,

$\zeta$  is the "zeta potential" of the particle, a quantity related to its charge (see, e.g. chapter 2 of "Zeta Potential in Colloid Science" by R.J. Hunter, Academic Press, 1981),

$\kappa^{-1}$  is the double-layer thickness (related to the electrolyte concentration; see above reference),

$a$  is the particle radius,

10  $V'/F'$  is the speed at which an uncharged sphere moves when acted on by an alternating force of unit magnitude, given by

$$V'/F' = \left| \pi p a^3 w \left\{ \frac{6v}{wa^2} + \frac{2i}{3} \left( 3 + \frac{2\Delta\rho}{\rho} \right) + 3\sqrt{2} (1+i) \sqrt{\frac{v}{wa^2}} \right\} \right|^{-1}$$

15

$\rho$  is the density of the suspending liquid,

$v$  is the kinematic viscosity of the suspending liquid, and

$\rho + \Delta\rho$  is the particle density.

20 by Finally, the quantities  $k$ ,  $\bar{a}$ ,  $b$  and  $c$  are defined

$$k = (i-1) \sqrt{\frac{w}{2v}}$$

$$\bar{a} = \frac{-3a}{2ik} e^{-ika}$$

25

$$b = -\frac{a^3}{2} \left( 1 - \frac{8}{ika} - \frac{3}{k^2 a^2} \right)$$

and

$$c = \frac{1 - i\omega'(1 - \epsilon_p/\epsilon)}{2 - i\omega'(2 + \epsilon_p/\epsilon)}$$

$\epsilon_p$  being the particle permittivity, and  
 $\omega' = \omega\epsilon/K^\infty$ ,

5 where  $K^\infty$  is electrolyte conductivity.

Finally,  $u(\zeta)$  is a function which is 0 when  $\zeta < 0$ ,  
 and 1 for  $\zeta > 0$

In the case when  $\kappa a \gg 1$  (thin double layer),  
 equation (4) reduces to

10

$$G = \frac{3aV'}{F'} (1 - i\kappa a)(1 + c). \quad (6)$$

Since  $(u(\zeta) - 1)$  depends on the sign, but not on  
 15 the magnitude of  $\zeta$ , and  $G$  is independent of  $\zeta$ , it follows  
 from equation (3) that the phase lag  $\arg \mu$  is also  
 independent of the magnitude of  $\zeta$ . This property of the  
 phase lag makes it ideal for the determination of particle  
 size. To illustrate this point reference is made to Figure  
 20 2 wherein  $\arg \mu$  for the  $\kappa a \gg 1$  case has been plotted as a  
 function of the non-dimensional variable  $\omega a^2/\nu$ .

Figure 2 was constructed using equation (6) with  
 parameters  $\Delta\rho/\rho = 1$ ,  $\epsilon_p/\epsilon = 0$ , and  $\zeta > 0$ .

From this figure it can be seen that for fixed  
 25 values of  $\omega$  and  $\nu$ ,  $\arg \mu$  increases monotonically with  
 increasing particle radius, tending to a limiting value of  
 $45^\circ$  as  $\omega a^2/\nu \rightarrow \infty$ .

With the aid of this curve it is possible to obtain a unique particle size from any measurement of  $\arg \mu$ . For example a phase lag of  $14^\circ$  implies that  $\omega a^2/\nu = 1$ . If the suspending liquid is water, which has a  $\nu$  value of  $.01 \text{ cm}^2/\text{sec}$ , and if the frequency of the applied field is 1 MHz, the particle radius corresponding to  $\omega a^2/\nu = 1$  is  $0.4 \mu\text{m}$ .

For a given solvent, the range of particle sizes which can be accurately measured in this way depends on the frequency of the applied field. From Figure 2 it can be shown that a one degree error in the measurement of  $\arg \mu$  leads to a relative error of less than 6% in the assessed particle size provided

$$1 < \omega a^2/\nu < 4.$$

Thus for any particle size, there is an optimum frequency range for size determination, given by

$$\nu/a^2 < \omega < 4\nu/a^2.$$

Although the curve in Figure 2 is only valid for a very limited class of suspension, the notion of an optimum frequency range is likely to have universal application. The precise end points of the range may vary from one suspension to the next, but the optimum will always be around  $\nu/a^2$ . For an  $0.1 \mu\text{m}$  particle in water  $\nu/a^2$  corresponds to a frequency of 16 MHz, while for a  $1 \mu\text{m}$



particle, this frequency is 160kHz.

From equation (3) it can be seen that  $\arg \mu$  changes by  $\pi$  radians (corresponding to  $180^\circ$  in phase lag), as the  $\zeta$  potential changes sign. Thus the curve of  $\arg \mu$  for  $\zeta < 0$  would have the same form as Figure 2, but with  $\arg \mu$  reduced by  $180^\circ$ . Since the total variation in  $\arg \mu$  with particle radius is only  $45^\circ$ , there is no possibility of a positive and a negative particle yielding the same phase angle.

In fact the sign of  $\zeta$  can be immediately ascertained from the quadrant in which the phase angle lies: the first quadrant indicates  $\zeta > 0$ , while the third quadrant implies  $\zeta < 0$ .

Once the radius  $a$  and the sign of  $\zeta$  have been ascertained from the phase lag,  $|\zeta|$  can be determined from the measured value of  $|\mu|$ . Figure 3 shows the variation of the non-dimensional quantity  $\rho v |\mu| / \epsilon |\zeta|$  with  $\omega a^2 / v$ .

Once again the curve comes from equation (6), with the same parameters as in Figure 2. From the curve it can be seen that  $|\mu|$  decreases monotonically with increasing frequency or particle radius. This curve can be used for determining  $|\zeta|$ . For example, if the particle radius has been found to be  $0.4 \mu\text{m}$  then from the figure  $\rho v |\mu| / \epsilon |\zeta| = 0.87$ . If the measured  $|\mu|$  is  $3.5 \times 10^{-4} \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ , it follows that  $|\zeta| = 50 \text{ mV}$  (assuming  $\rho$ ,  $v$  and  $\epsilon$  values for water). Since the phase lag measurement indicated a positive  $\zeta$ , it is found that  $\zeta = 50 \text{ mV}$ .

Although Figures 2 and 3 were obtained with the formula (6) for the thin double layer case, the procedure herein described is valid for arbitrary double layer thickness. To summarize the main points:

5 (1) The particle size and the sign of  $\zeta$  can be obtained from phase lag measurement.

(2)  $|\zeta|$  can then be obtained from the measured  $|\mu|$  value.

(3) The optimum sizing frequencies are around  
10  $w = v/a^2$ .

## 2. Results valid for more general suspensions.

The formula (1) defining the electrophoretic mobility can also be applied to a much more general class of suspensions, namely "statistically isotropic" suspensions.  
15 These are suspensions which appear to be isotropic, from the macroscopic point of view (Batchelor, G.K., J. Fluid Mech., 41, 545, (1970)). Many suspensions fall into this category, particularly if they have not been subjected to a flow and if sedimentation is not too significant.

20 Since these isotropic suspensions may be concentrated, the particle interactions will cause the velocity to vary from one particle to the next. The quantity  $\bar{V}_0$  which appears in equation (1) in this case is intended to represent an average of the particle velocities  
25 given by

$$\bar{V}_0 = \frac{\sum_{j=1}^N \bar{V}^j \Delta m^j}{\sum_{k=1}^N \Delta m^k}$$

where  $\underline{v}_e^{j\text{wt}}$  is the velocity of the centre of mass of the  $j$ th particle in the sample, and  $\Delta m^j$  is the particle mass minus the mass of solvent displaced by the particle.

The applied field  $E_0$  also represents an average, namely an average of the local electric field over a representative volume of the suspension (see the previous reference). For a dilute suspension this is equivalent to the previous definition.

The notion of electrophoretic mobility is considerably more complicated for "non-isotropic" suspensions. In these suspensions the velocity  $\underline{v}_0$  is not usually parallel to the applied field. Thus if the applied field is parallel to the  $x$  axis of some cartesian coordinate system, the particle velocity will in general have components along the  $x, y$  and  $z$  axes. Since the velocity is still proportional to field strength, it is possible to define three electrophoretic mobilities, one for each component of  $\underline{v}_0$ . Three more components are required to characterize the mobility with a field in the  $y$  direction, and another three for a field in the  $z$  direction, giving nine in all.

It is convenient to regard these nine mobilities as the components of a single entity known as the "electrophoretic mobility tensor", denoted by  $\underline{\mu}$ . The nine components of  $\underline{\mu}$  are usually set out in the  $3 \times 3$  matrix

$$\begin{vmatrix} \mu_{11} & \mu_{12} & \mu_{13} \\ \mu_{21} & \mu_{22} & \mu_{23} \\ \mu_{31} & \mu_{32} & \mu_{33} \end{vmatrix},$$

5 where  $(\mu_{11}, \mu_{21}, \mu_{31})E$  are the x, y and z components of  $\underline{v}_0$  caused by a field along the x-axis. The other two columns of the matrix give the velocity due to fields in the y and z directions respectively.

In this notation, the relationship between  $\underline{v}_0$  and  $\underline{E}_0$  for a non-isotropic suspension takes the compact form

$$\underline{v}_0 = \underline{\mu} \cdot \underline{E}_0$$

In the case of an isotropic suspension, the off-diagonal entries in the  $\underline{\mu}$  matrix are zero, and the diagonal entries take the common value denoted earlier by  $\mu$

15 The above result reduces to (1) in this case.

The components of  $\underline{\mu}$  will depend on the particle size and charge distribution. Unfortunately the exact calculation of this relationship is only feasible at present for dilute suspensions of particles of simple geometry. For the more complicated types of suspensions which are likely to be encountered in practice, there appear to be two options for obtaining approximate relations between size, charge and mobility.

#### (a) Cell Models

25 If the particles are not elongated or flat it should be possible to approximate them by spheres. In a cell model the effect of neighbouring particles on any given

sphere is assumed to be the same as an outer spherical surface centred on that particle. The "cell" then consists of a single particle surrounded by a concentric spherical surface, with the annular region between occupied by electrolyte. Such models have been successfully used in the calculation of average sedimentation velocities (see "Low Reynolds Number Hydrodynamics" by Happel and H. Brenner, Prentice-Hall, (1965)) and in the calculation of electrophoretic mobilities (Levine S. and Neale G., J. Colloid. Interface Sci. 47, 520 (1974)) in steady electric fields, for concentrated suspensions. The boundary conditions to be applied at the outer surface of the cell depend on the problem at hand. The boundary conditions suggested here are: zero total force, zero pressure, zero perturbation in ion densities, and an electric potential equal to  $-E_0 \cdot \underline{x}$ , where  $\underline{x}$  is the position vector measured from the particle centre. These boundary conditions may require some modification in the light of future experimental studies.

20 (b) An empirical approach

If the cell model is not appropriate for the suspension of interest, an empirical approach can be adopted. In this approach, samples of the suspension are removed and analysed after each set of mobility measurements is made. These mobility measurements should be carried out over a range of frequencies spanning the optimum range corresponding to the expected particle size range. Changes

in the particle size or  $\zeta$  potential distribution can then be correlated with the form of the curves of  $|\mu_{ij}|$  and  $\arg |\mu_{ij}|$  as a function of frequency, where the symbol  $\mu_{ij}$  denotes any measured component of the mobility tensor.

- 5 For suspensions in which the  $\zeta$ -potential is both uniform and small,  $\mu$  will be proportional to  $\zeta$ . As a consequence the quantities  $\arg \mu_{ij}$  will be independent of the magnitude of  $\zeta$ , as we saw in the dilute suspension of spheres in §1. Although  $\arg \mu$  may depend on  $|\zeta|$  for more  
10 general suspensions, it is still likely that of the two quantities  $|\mu|$  and  $\arg |\mu|$ , the latter will be the more sensitive function of particle size. Thus in attempting to correlate mobility with particle size distribution, attention should be focussed on  $\arg \mu$  rather than  $|\mu|$ .
- 15 3. The experimental determination of the electrophoretic mobility

Turning now to the second major aspect of the invention: the means by which the electrophoretic mobility can be measured experimentally.

- 20 In this section there is described a general class of devices which can be used for making these measurements, and how the mobility can be determined from the various measured quantities.

The results given in this section apply to any  
25 colloid, except in those instances where statistically isotropic colloids are specifically referred to.

The devices for measuring the mobility consist of

a "cell" which contains the suspension, together with various means for measuring voltage differences (or electric currents) and pressure differences across the cell, and means for generating sound waves and/or alternating electric  
5 fields in the cell.

To take a simple example, the cell could consist of two parallel metal plates with the suspension filling the gap between them. Later in this section it will be shown how the mobility can be determined for such a cell from the  
10 measurement of the pressure difference and open circuit voltage difference generated between the plates by the vibration of one of those plates.

As may be gathered from the above description, the electrophoretic mobility is measured when both sound  
15 waves and electric fields are present in the suspension. In addition to its effect on particle motion, the electric field generates electric currents in the suspension. The sound waves also generate electric currents, due to the fact that both particles and solvent carry a charge, and the  
20 particle motions in the sound wave are different from that of the liquid, owing to the particle inertia. The total current density due to the electric field and the sound waves is given by an expression of the form

$$25 \quad i_o = \frac{\sigma}{\omega} \nabla p_o + \frac{K^*}{\omega} E_o \quad (6)$$

Here  $i_o e^{i\omega t}$  is the volume-averaged current density, a quantity which includes both free charge and electric

displacement contributions (see O'Brien, R.W., Adv. Coll. Interface Sci., 16, 281, (1982)).  $v_{p_0} e^{i\omega t}$  is the macroscopic pressure gradient due to the sound waves, and  $\underline{\alpha}$  and  $\underline{\kappa}^*$  are properties of the suspension,  $\underline{\kappa}^*$  being called the "complex conductivity tensor". Equation (6) has not appeared before in the scientific literature.

The quantity  $\underline{\alpha}$ , which characterizes the current due to the sound waves, is related to the electrophoretic mobility tensor by the formula

$$\underline{\alpha} = \frac{\phi \Delta \rho}{\rho} \underline{\mu}^T, \quad (7)$$

where  $\phi$  is the volume fraction of the suspension occupied by particles, and as before  $\rho$  is the solvent density, and  $\rho + \phi \Delta \rho$  is the suspension density:  $\underline{\mu}^T$  is the "transpose" of the mobility tensor, the quantity whose components are obtained by interchanging the rows and columns of the  $\underline{\mu}$  matrix.

With the aid of (7) it is possible to determine  $\underline{\mu}$  once  $\underline{\alpha}$  is known. The devices described here determine  $\underline{\mu}$  by measuring  $\underline{\alpha}$ .

In order to provide examples of ways in which  $\underline{\mu}$  can be measured using this class of device, reference is made to the parallel plate cell, illustrated in Figure 4.

The separation  $h$  between the plates is assumed to be much smaller than the width and height of the plates. Sound waves are set up in the device by the forced oscillation of one of the plates. The resulting pressure



difference across the plates  $\Delta p e^{i\omega t}$  is measured by, for example transducers on the plates, and the open circuit voltage difference  $\Delta \psi e^{i\omega t}$  is also measured.

In such a device the current  $i_0$  in the suspension is uniform. In order for such a current to flow, the plates must be linked by a wire to complete the circuit. Under open-circuit conditions the current  $i_0$  is therefore zero everywhere in the suspension. Thus equations (6) gives

$$\alpha \nabla p_0 = -K^* E_0$$

where, for simplicity the suspension is taken to be isotropic. Integrating this result across the plates, it is found that

$$\alpha \Delta P = K^* \Delta \psi$$

Thus if  $K^*$  has been determined from a conductivity measurement,  $\alpha$  can be obtained from the measurement of  $\Delta P$  and  $\Delta \psi$ .

Alternatively, if the two plates are short circuited the electric field in the suspension will be zero, and (6) reduces to

$$i_0 = \alpha \nabla p_0$$

for an isotropic suspension. Integrating across the plates

and using the fact that  $\underline{i}_0$  is uniform it is found that

$$\alpha = \frac{I_0 h}{A \Delta P}$$

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where  $A$  is the plate area, and  $I_0 e^{i\omega t}$  is the current passing between the plates. Thus by measuring the pressure difference and short-circuit current it is possible to determine without the need for a conductivity measurement.

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The mathematical formula for obtaining  $\underline{\alpha}$  for a general device is derived with the aid of the result

$$\nabla \cdot \underline{i}_0 = 0,$$

which holds everywhere in the suspension. Integrating equation (6) over the volume  $v$  of the suspension within the cell, and using the above identity, it is found that

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$$\int_A \underline{x} \cdot \underline{i}_0 \cdot \underline{n} dA = \underline{\alpha} \int_A p_0 \underline{n} dA - K^* \int_A \psi \underline{n} dA, \quad (8)$$

20 where  $z$  denotes the surface of  $v$  and  $\underline{n}$  is the unit normal directed outwards from  $v$ .  $\underline{x}$  is the position vector to the surface from an arbitrary point in the suspension, and  $\psi e^{i\omega t}$  is the electrical potential.

From equation (8) it can be seen that components of  $\underline{\alpha}$  can be determined if  $\underline{i}_0 \cdot \underline{n}$ ,  $p_0$  and  $\psi$  are known over the surface of  $v$ . In the parallel plate device referred to above, either  $\underline{i}_0 \cdot \underline{n}$  (open-circuit) or  $\psi$  (short-circuit) were

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set to zero, and the other two quantities measured.

As mentioned in §2, it is envisaged that the devices described here would make measurements over a range of frequencies appropriate to the expected particle size range.

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Previous known devices are manufactured by Matec Instruments, Warwick, R.I., U.S.A. and Pen Kem, Inc., Bedford Hills, N.Y., U.S.A. The Matec device measures sound waves generated by electric fields, and electric fields generated by sound waves at about 1MHz, in a parallel plate cell. The device measures the potential, but not the pressure difference across the cell. It is therefore not suited to the direct determination of  $\underline{g}$ .

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The Pen-Kem instrument measures the potential difference between two electrodes caused by the generation of sound waves at around 200 kHz. The device also measures the pressure at a point some distance away from the electrodes. As it is not possible to directly determine the pressure difference between the electrodes from this single pressure measurement, this device is also unsuited to the direct determination of  $\underline{g}$ .

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Apparatus according to the present invention measures the interaction of sound waves and electric fields over a range of frequencies, and comprises means to convert the information so obtained to provide a direct measurement of electrophoretic mobility, from which particle size and zeta potential can be inferred.

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Although the invention has been described above with reference to examples and to preferred embodiments, it will be appreciated that the invention may be embodied in other forms or carried out in other ways without departing  
5 from the spirit or essential characteristics thereof. The above description is therefore to be considered in all respects, illustrative and not restrictive, and all changes which come within the meaning and range of equivalency are intended to be embraced therein.

CLAIMS

1. A method for determining the size and charge of particles dispersed in a fluid medium from the phase lag and amplitude of particle velocity in an alternating electric field.
2. A method for determining the particle size in a fluid medium having uniform, low  $\zeta$  potential from a measurement of the phase of the particle motion in a high frequency alternating electric field, and wherein the zeta-potential can be determined from the amplitude of the motion in the alternating field.
3. A method for determining the average size and charge of particles in a fluid medium by combining measurements of the phase and amplitude of the particle motion in an electric field with an appropriate cell model.
4. A method for determining size and charge for polydisperse suspensions by a correlation technique, involving measurements of the average particle velocity over a range of frequencies, and determining the appropriate frequency range from the expected particle size range.
5. A method for obtaining the particle velocity in an alternating electric field from measurements of the interaction of sound waves and electric fields in the suspension.
6. A method for generating and measuring the interaction of sound waves and electric fields in fluid suspension comprising positioned spaced apart electrodes and

pressure transducers in contact with the suspension, enabling the simultaneous measurement of electrical potentials, currents and pressure differences in the suspension.

7. Apparatus for determining the particle size and charge of particles dispersed in a fluid medium when using a method as claimed in any one of the previous claims.

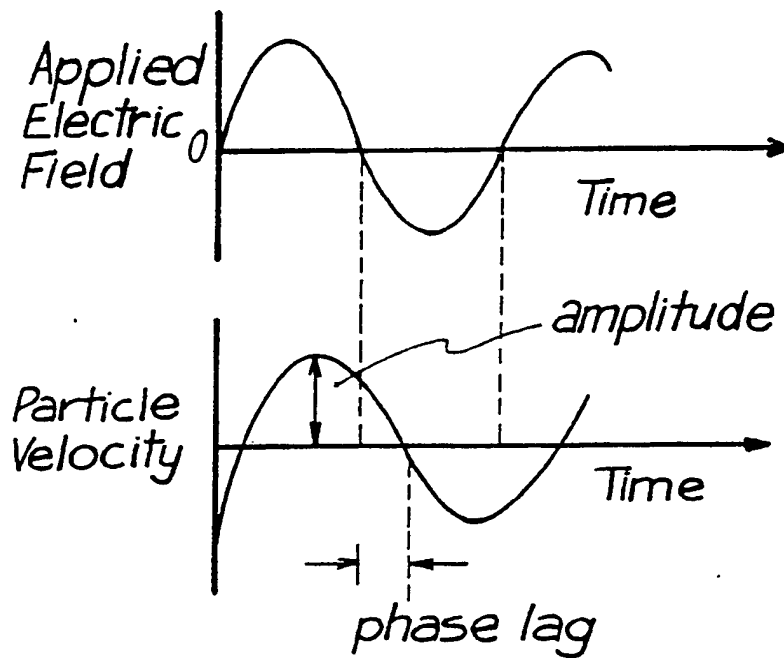


FIG.1

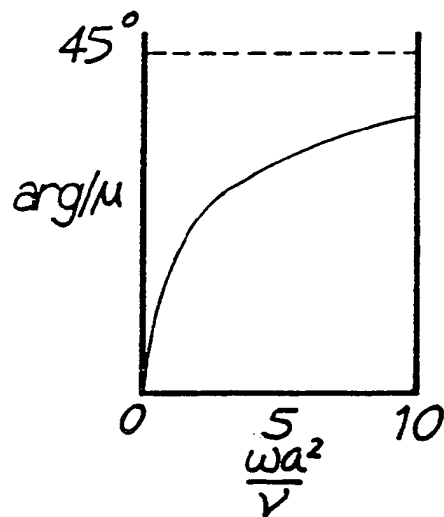


FIG.2

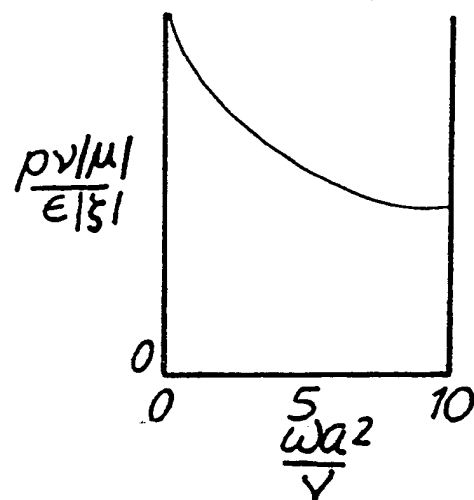
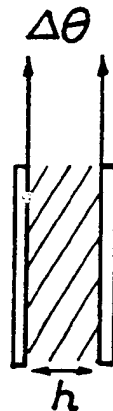


FIG.3

FIG.4



# INTERNATIONAL SEARCH REPORT

International Application No PCT/AU 87/00333

## I. CLASSIFICATION OF SUBJECT MATTER (The search classification symbols apply, in addition to the classification symbols of the International Patent Classification (IPC) or to both National Classification and IPC)

Int. Cl.<sup>4</sup> G01N 15/02, 27/26, 29/02; G01R 29/24; G01P 5/08

## II. FIELDS SEARCHED

Minimum Documentation Searched \*

Classification System

Classification Symbols

IPC G01N 15/02, 27/26, 27/28, 27/60, 29/02; G01R 29/24;  
G01P 5/08

Documentation Searched other than Minimum Documentation  
to the extent that such documents are included in the fields searched \*

AU : IPC as above

## III. DOCUMENTS CONSIDERED TO BE RELEVANT \*

Category \* : Citation of Document, \*\* with indication, where appropriate, of the relevant passages \*\* ; Relevant to Claim No. \*\*

P,X	US,A, 4633714 (MAZUMDER et al) 6 January 1987 (06.01.87)	(1,7)
X	US,A, 4497208 (OJA et al) 5 February 1985 (05.02.85)	(5,6)
A	GB,A, 1185898 (COULTER ELECTRONICS LIMITED) 25 March 1970 (25.03.70)	(1)
A	US,A, 4375673 (LEWIS et al) 1 March 1983 (01.03.83)	(1)
A	WO,A, 86/00707 (FORSCHUNGSANWENDUNGSGESELLSCHAFT M.B.H.) 30 January 1986 (30.01.86)	(2)
A	WO,A, 86/02727 (LIFFLER) 9 May 1986 (09.05.86)	(4)
A	US,A, 3633415 (LUCE) 11 January 1972 (11.01.72)	(5)

\* Special categories of cited documents: \*\*

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

- "X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step

- "Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

- "Z" document member of the same patent family

## IV. CERTIFICATION

Date of the Actual Completion of the International Search  
12 January 1988 (12.01.88)

Date of Mailing of this International Search Report

(27.01.88) 27 JANUARY 1988

International Searching Authority

Australian Patent Office

Signature of Authorized Officer

R. MURRAY



## FURTHER INFORMATION CONTINUED FROM THE SECOND SHEET

V. ☐ OBSERVATIONS WHERE CERTAIN CLAIMS WERE FOUND UNSEARCHABLE

This international search report has not been established in respect of certain claims under Article 17(2) (a) for the following reasons:

1. ☐ Claim numbers ..... because they relate to subject matter not required to be searched by this Authority, namely:
  
2. ☐ Claim numbers ..... because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically
  
3. ☐ Claim numbers ..... because they are dependent claims and are not drafted in accordance with the second and third sentences of PCT Rule 6.4(a).

VI. ☒ OBSERVATIONS WHERE UNITY OF INVENTION IS LACKING

This International Searching Authority found multiple inventions in this international application as follows:

Claims 1-3 are directed to measuring particle charge and size in an electric field whereas claim 4 is directed to measuring charge and size by measuring particle velocities over a range of frequencies, and Claims 5 and 6 are directed to measuring the interaction of sound waves and electric fields.

1. ☒ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims of the international application.
2. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims of the international application for which fees were paid, specifically claims:
  
3. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claim numbers:
  
4. ☐ As all searchable claims could be searched without effort justifying an additional fee, the International Searching Authority did not invite payment of any additional fee.

## Remarks on Protest

- ☒ The additional search fees were accompanied by applicant's protest.
- ☐ No protest accompanied the payment of additional search fees.

ANNEX TO THE INTERNATIONAL SEARCH REPORT ON  
INTERNATIONAL APPLICATION NO. PCT/AU 87/00333

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent Document Cited in Search Report	Patent Family Members			
US 4633714	EP	214769		
US 4497208	EP	129766	JP	60015554
US 4375673	GB	2083619	JP	57079958
WO 8600707	AU	46027/85	EP	225322
WO 8602727	DE	3438798	EP	199774
			US	4706509